

**Circulating Currents in Parallel Generator Applications (Rev. A13)**



Quantities are per unit percentage unless otherwise specified  
 All units assumed to have the same base voltage

**Project data:**

Project Name: Sample DPNL Simulation  
 Project Description: 2 x 800kW existing 0.8667 pitch, 1 x 800kW new 0.6667 pitch  
 Prepared by:  
 Date:

Comments:

Base Values:

Frequency:	60	Hz
Generator base voltage (L-L):	480	V
phase voltage (L-N):	277	V
Total kVA:	3750.0	kVA
Current:	4510.5	A (bus)

Similar pitch parallel machines ("Y" side)

Generator Pitch	Ratings					Z_base ohm	
	Power kW	PF	Apparent kVA	Voltage V	Current A		
Gen 1:	2/3	800	0.800	1000.0	480	1202.8	0.2304
Gen 3:							
Gen 5:							
Gen 7:							
Gen 9:							
Gen 11:							

	Reactances at fundamental frequency ("Y" side)											
	Zero Sequence X0				Negative Sequence X2				Subtransient X"d			
	Unsaturated		Saturated		Unsaturated		Saturated		Unsaturated		Saturated	
	%p.u.	ohm	%p.u.	ohm	%p.u.	ohm	%p.u.	ohm	%p.u.	ohm	%p.u.	ohm
Gen 1:	0.95%	0.0022	0.95%	0.0022	11.41%	0.0263	11.41%	0.0263	10.94%	0.0252	10.94%	0.0252
Gen 3:												
Gen 5:												
Gen 7:												
Gen 9:												
Gen 11:												
3 x fund:		0.0066		0.0022		0.0789		0.0263		0.0756		0.0252

Equivalent Reactances "Y" side			
Unsaturated (X0+X2+X"d)/3		Saturated (X0+X2+X"d)/3	
%p.u.	ohm	%p.u.	ohm
7.77%	0.0179	7.77%	0.0179
at fund freq	0.0179	at fund freq	0.0179
at 3 x fund	0.0537	at 3 x fund	

Bus kVA: 1000.0 kVA  
 Isc: kA  
 Isc\_3Ph: kA

SOURCE Calculation

Second set of similar pitch parallel machines or other Source (different than the above) ("Z" side). Only this side can be used as solidly grounded Utility Transformer!

		Ratings					
Generator Pitch	Power kW	PF	Apparent kVA	Voltage V	Current A	Z_base ohm	
Gen 2:	13/15	800	0.800	1000.0	480	1202.8	0.2304
Gen 4:	13/15	800	0.800	1000.0	480	1202.8	0.2304
Gen 6:							
Gen 8:							
Gen 10:							
Gen 12:							

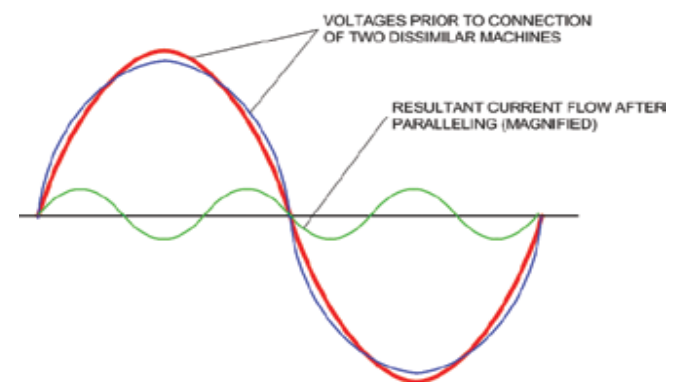
Reactances at fundamental frequency ("Z" side)												
Zero Sequence X0				Negative Sequence X2				Subtransient X'd (***)				
Unsaturated		Saturated		Unsaturated		Saturated		Unsaturated		Saturated		
%p.u.	ohm	%p.u.	ohm	%p.u.	ohm	%p.u.	ohm	%p.u.	ohm	%p.u.	ohm	
Gen 2:	10.33%	0.0238	10.33%	0.0238	15.67%	0.0361	15.67%	0.0361	15.49%	0.0357	15.49%	0.0357
Gen 4:	10.33%	0.0238	10.33%	0.0238	15.67%	0.0361	15.67%	0.0361	15.49%	0.0357	15.49%	0.0357
Gen 6:												
Gen 8:												
Gen 10:												
Gen 12:												
3 x fundamental:		0.0119	0.0119	0.0181	0.0181	0.0178	0.0178	0.0178	0.0178	0.0178	0.0178	0.0178
		0.0357		0.0542		0.0535						
("Y"  "Z"):		0.0018	0.0018	0.0107	0.0107	0.0104	0.0104	0.0104	0.0104	0.0104	0.0104	0.0104
		0.0055		0.0321		0.0313						

(\*\*\*) For Transformer as a parallel source the Subtransient Reactance value is used as the Positive-Sequence Reactance X1

Equivalent reactances "Z" side			
Unsaturated (X0+X2+X'd)/3		Saturated (X0+X2+X'd)/3	
%p.u.	ohm	%p.u.	ohm
13.83%	0.0319	13.83%	0.0319
13.83%	0.0319	13.83%	0.0319
at fund freq	0.0159	at fund freq	0.0159
at 3 x fund	0.0478	at 3 x fund	
Parallel imp:	0.0077	Parallel imp:	0.0077
at 3 x fund:	0.0230	at 3 x fund:	
	0.0084		0.0084
	0.0253		

Bus kVA: 2000.0 kVA  
 Isc: kA  
 Isc\_3ph: kA

When generators are paralleled, the voltages of the two machines are forced to the exact same magnitude at the point where they are connected to the paralleling bus. Differences in instantaneous waveforms of electromotive force (emf) generated by the alternators will result in current flow from the machine with higher instantaneous emf to the machine(s) with lower instantaneous emf. Voltage waveform lines cross each other three times in each half cycle, therefore the current generated appears as a triple of the fundamental frequency current (third-order harmonic).



### Circulating Current Calculation

Assumption:

Select an instantaneous voltage difference that is estimated by generator manufacturer:

Instantaneous voltage difference is at 3 x fundamental:

$V_{g1} - V_{g2} = 10$  V      3.6% [%p.u.]      180 Hz

Circulating phase current at 3 x fundamental:

$I_{cir} = 237$  A

Circulating neutral current at 3 x fundamental:

$I_{cir\_N} = 710$  A

DPNL Calculation

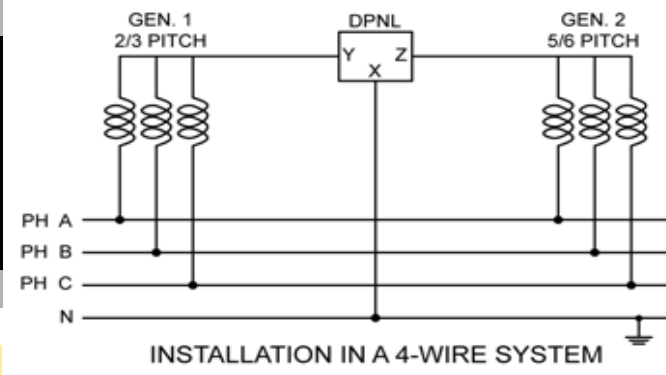
with application of GenLink DPNL							
DPNL Ratings			Z_base ohm	"Shoulder"			"Circ. Path"
Voltage V	Current A Return   Circ.			DPNL Zero-Seq X.yx mH   %p.u.   ohm			X.yz ohm
480	1500	750	0.3695	0.044	4.49%	0.0166	0.0662
DPNL saturation factor:			7	at 3 x fundamental: DPNL X_sat:			0.0498   0.20 0.0024

Circulating phase current with DPNL at 3 x fundamental:

I\_cir = 15.7 A 15.1 reduction

Circulating neutral current with DPNL at 3 x fundamental:

I\_cir\_dpnl = 47.0 A 15.1 reduction



Fault\_DPNL Calculation

S_base =	3750	kVA	three-phase apparent power base
V_base =	480	V	line-to-line voltage base
I_base =	4510.5	A	current base
Z_base =	0.0614	ohm	impedance base

**Fault Current Calculation for each side**

No NGL:

	"Y" side			"Z" side			
Z_eq:	0.0179	ohm	0.29 p.u.	0.0159	ohm	0.26 p.u.	Equivalent impedance
X1_eq:	0.0252	ohm	0.41 p.u.	0.0178	ohm	0.29 p.u.	Equivalent positive-sequence reactance
3-ph fault (Isc_3ph):	10.99	kA	2.44 p.u.	15.53	kA	3.44 p.u.	Estimated 3-phase fault current
ground fault (Isc):	15.49	kA	3.43 p.u.	17.39	kA	3.86 p.u.	Estimated line-to-ground fault current

**Fault Current Calculation of parallel sources**

No NGL:

Z_eq:	0.0084	ohm	0.14 p.u.	Equivalent impedance of parallel sources
X1_eq:	0.0104	ohm	0.17 p.u.	Equivalent positive-sequence reactance of parallel sources

Three-phase fault is balanced, no negative- or zero-sequence current components are present

3-ph fault (Isc_3ph):	26.52	kA	5.88 p.u.	Estimated 3-phase fault current at the generators terminals
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Single-phase fault: all three positive-, negative-, and zero-sequence current components are present

ground fault (Isc):	32.88	kA	7.29 p.u.	Estimated line-to-ground fault current at the generators terminals
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(a) Solidly

**Fault Current Calculation with DPNL**

With DPNL:

	"Y" side			"Z" side			
Z_eq:	0.0250	ohm	0.41 p.u.	0.0230	ohm	0.38 p.u.	Equivalent impedance
X1_eq:	0.0252	ohm	0.41 p.u.	0.0178	ohm	0.29 p.u.	Equivalent positive-sequence reactance
3-ph fault (Isc_3ph):	10.99	kA	2.44 p.u.	15.53	kA	3.44 p.u.	Estimated 3-phase fault current
ground fault (Isc):	11.08	kA	2.46 p.u.	12.03	kA	2.67 p.u.	Estimated line-to-ground fault current

**Fault Current Calculation of parallel sources with DPNL**

with NGL

Z_eq:	0.0120	ohm	0.20 p.u.	Equivalent impedance of parallel sources
X1_eq:	0.0104	ohm	0.17 p.u.	Equivalent positive-sequence reactance of parallel sources

Three-phase fault is balanced, no negative- or zero-sequence current components are present

3-ph fault (Isc_3ph):	26.52	kA	5.88 p.u.	Estimated 3-phase fault current at the generators terminals
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Single-phase fault: all three positive-, negative-, and zero-sequence current components are present

ground fault (Isc):	23.11	kA	5.12 p.u.	Estimated line-to-ground fault current at the generators terminals
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Note: DPNL and/or NGL application does not affect three-phase fault.

### Effective Grounding Calculation

No DPNL:

	"Y" side	"Z" side		
$X_1$ :	<b>0.0252</b>	<b>0.0178</b>	ohm	sub-transient reactance of the generator
$X_0$ :	<b>0.0022</b>	<b>0.0119</b>	ohm	zero-sequence reactance of the generator
$X_0/X_1$ ratio:	<b>0.0868</b>	<b>0.6669</b>	< 3 ? is	<b>effectively grounded</b>

### Individual NGI Effective Grounding Calculation

With NGI in each generator neutral:

$X_1$ :	<b>0.0252</b>	<b>0.0178</b>	ohm	sub-transient reactance of the generator
$X_0$ with NGI:	<b>0.0232</b>	<b>0.0169</b>	ohm	zero-sequence reactance of the generator with DPNL
max. allowable $X_0$ :	<b>0.0756</b>	<b>0.0535</b>	ohm	maximum allowable zero-sequence reactance
$X_0/X_1$ ratio:	<b>0.9201</b>	<b>0.9491</b>	< 3 ? is	<b>effectively grounded</b>

### DPNL Effective Grounding Calculation

With DPNL in the neutral:

$X_1$ :	<b>0.0252</b>	<b>0.0178</b>	ohm	sub-transient reactance of the generator
$X_0$ with DPNL:	<b>0.0046</b>	<b>0.0143</b>	ohm	zero-sequence reactance of the generator with DPNL
max. allowable $X_0$ :	<b>0.0756</b>	<b>0.0535</b>	ohm	maximum allowable zero-sequence reactance
$X_0/X_1$ ratio:	<b>0.1808</b>	<b>0.7997</b>	< 3 ? is	<b>effectively grounded</b>

### DPNL + NGI Effective Grounding Calculation

With DPNL + NGI in the neutral:

$X_1$ :	<b>0.0252</b>	<b>0.0178</b>	ohm	sub-transient reactance of the generator
$X_0$ with DPNL+NGI:	<b>0.0022</b>	<b>0.0143</b>	ohm	zero-sequence reactance of the generator with DPNL + NGI
max. allowable $X_0$ :	<b>0.0756</b>	<b>0.0535</b>	ohm	maximum allowable zero-sequence reactance
$X_0/X_1$ ratio:	<b>0.0868</b>	<b>0.80</b>	< 3 ? is	<b>effectively grounded</b>